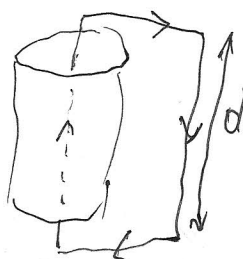


$$\vec{K} = n \cdot d \cdot I \hat{e}_\varphi$$

$$\vec{B} = B \hat{e}_z \text{ i tylko dla } r < R$$



$$\oint \vec{B} \cdot d\vec{l} = B_z \cdot d$$

$$\oint \mu_0 \vec{j} \cdot d\vec{s} = \mu_0 n d I \cdot d$$

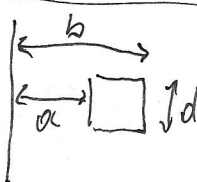
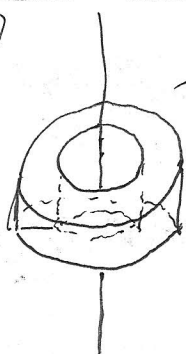
$$B_z = \mu_0 I n$$

Strumień przez nd pierścieni

$$\iint \vec{B} \cdot d\vec{s} = \mu_0 I n \cdot n d \cdot \pi R^2 \rightarrow$$

$$L = \frac{\iint \vec{B} \cdot d\vec{s}}{d \cdot I} = \mu_0 n^2 \cdot \pi R^2$$

2a)



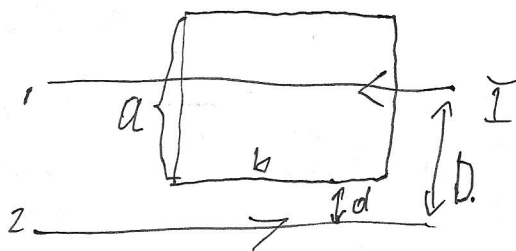
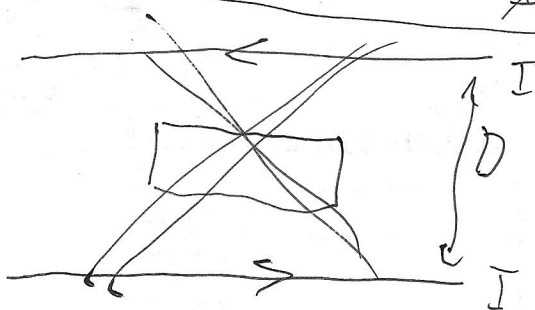
$$L_{12} = \frac{\iint \vec{B}_2 \cdot d\vec{s}_1}{I_2}$$

1 - toroid
2 - drut (bo całkowita z pow. druta to magia)

pole drutu: $2\pi r B_2 = \mu_0 I_2 \rightarrow B_2 = \frac{\mu_0 I_2}{2\pi r}$

$$L_{12} = \int_a^b dr \int_0^d dz \cdot \frac{\mu_0 I_2}{2\pi r} \cdot N = \frac{\mu_0 d N}{2\pi} \ln \frac{b}{a}$$

2b)



Pole od dwóch drutów: $B = B_1 + B_2 = \frac{\mu_0 I}{2\pi(D-r)} + \frac{\mu_0 I}{2\pi r}$

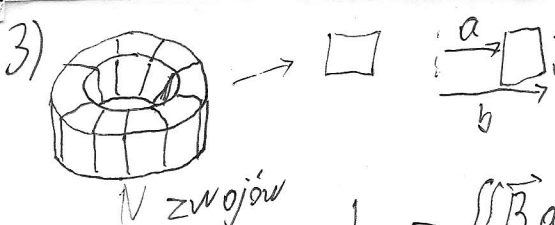
dla druta 1 za pomocą symetrii pola:

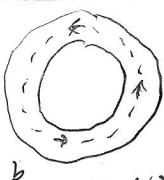
~~dla druta 1~~ $B_1(D+dr) = -B_1(D-dr) \Rightarrow \int_{D-dr}^{D+dr} \vec{B}_1 \cdot d\vec{s} = 0 \Rightarrow \iint \vec{B}_1 \cdot d\vec{s}$

ma zmniejszone granice

$$\iint \vec{B}_1 \cdot d\vec{s} = \frac{\mu_0 I}{2\pi} \int_0^b dz \int_d^{2D-d-a} \frac{1}{D-r} = \left| \frac{w=D-r}{dw=-dr} \right| = \frac{\mu_0 I b}{2\pi} \int_{d+a-D}^{D-d} \frac{dw}{w} = \frac{\mu_0 I b}{2\pi} \ln \frac{D-d}{d+a-D}$$

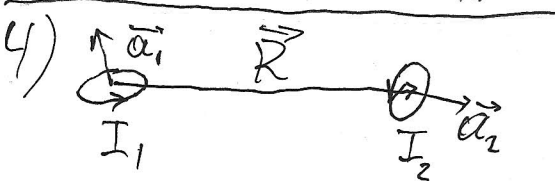
$$\iint \vec{B}_2 \cdot d\vec{s} = \frac{\mu_0 I b}{2\pi} \ln \frac{d+D}{d} \rightarrow L = \frac{\iint \vec{B} \cdot d\vec{s}}{I} = \frac{\mu_0 b}{2\pi} \ln \frac{D^2 - d^2}{d^2 + ad - dD}$$

3)  N zwojów

Amper:  $2\pi r B_\varphi = \mu_0 N I$
 $B = \frac{\mu_0 N I}{2\pi r}$

$$L = \frac{\iint \vec{B} d\vec{s}}{I} = \frac{N \cdot \int_a^b dz \int_a^b dr \frac{\mu_0 N I}{2\pi r}}{I} = \frac{\mu_0 N^2 d}{2\pi} \ln \frac{b}{a}$$

$$W = \frac{L I^2}{2} = \frac{\mu_0 I^2 N^2 d}{4\pi} \ln \frac{b}{a}$$

4)  $\vec{B}_{dip} = \frac{\mu_0}{4\pi r^3} (3(\vec{m} \cdot \vec{r})\vec{r} - \vec{m}|\vec{r}|^2)$, $\vec{m} = I \cdot \vec{a}$

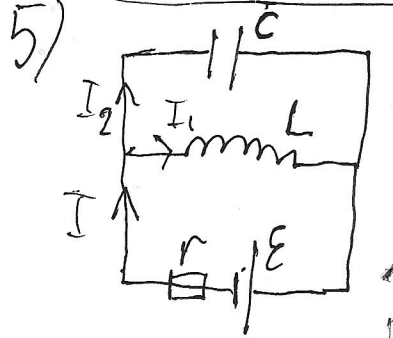
R jest bardzo duże, więc pole przy całym dipolu jest takie samo

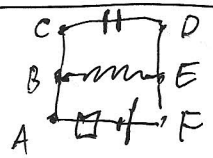
$$L = \frac{\iint \vec{B}_1 d\vec{s}_2}{I_1} = \frac{\mu_0}{4\pi R^3} [3(\vec{a}_1 \cdot \vec{R}) \cdot \vec{R} - \vec{a}_1 |\vec{R}|^2] \cdot \vec{a}_2 = \frac{\mu_0 [3(a_1 R)(a_2 R) - (a_1 a_2) R^2]}{4\pi R^3}$$

$$\frac{\partial W}{\partial t} = -\mathcal{E}_2 \cdot I_1 = \partial_t (L \cdot I_2) I_1 \rightarrow W = L \cdot I_1 I_2 = \frac{\mu_0 [3(\vec{m}_1 \cdot \vec{R})(\vec{m}_2 \cdot \vec{R}) - (\vec{m}_1 \cdot \vec{m}_2)(\vec{R} \cdot \vec{R})]}{4\pi R^3}$$

przypomnienie: prawa Kirchhoffa

1 → w każdym węźle $\sum I_m = 0$	 $U = I \cdot R$  $U = \frac{Q}{C} = \frac{\int I dt}{C}$  $U = L \cdot \partial_t I$ spadki napięć siła elektromotoryczna
2 → w każdym oczku $\sum U = \sum \mathcal{E}$	

5)  $I = I_1 + I_2$

 Oczka: BCDE, ACDF, ABFE

ACDF: $\frac{Q_2}{C} + I r = \mathcal{E} \rightarrow Q_2 = -I r C + \mathcal{E} C$

BCDE: $\frac{Q_2}{C} - L \partial_t I_1 = 0$

ABFE: $I r + L \partial_t I_1 = \mathcal{E}$

wystarczy 2 równania

$$\partial_t Q_2 = I_2 = C \cdot \partial_t^2 I_1 \quad (\text{z BCDE})$$

$$I r + L \cdot \partial_t I_1 = I_1 r + r C L \cdot \partial_t^2 I_1 + L \cdot \partial_t I_1 = \mathcal{E}$$

$$\partial_t^2 I_1 + \frac{1}{r C} \partial_t I_1 + \frac{1}{L C} I_1 = \frac{\mathcal{E}}{R L C}$$

najpierw równanie jednorodne:

$$\partial_t^2 I_1 + \frac{1}{rC} \partial_t I_1 + \frac{1}{LC} I_1 = 0 \rightarrow I_1 = A_1 e^{\lambda_1 t} + B_1 e^{\lambda_2 t}$$

$$\partial_t^2 (A e^{\lambda t}) + \frac{1}{rC} \partial_t (A e^{\lambda t}) + \frac{1}{LC} A e^{\lambda t} = A e^{\lambda t} \left(\lambda^2 + \frac{\lambda}{rC} + \frac{1}{LC} \right) = 0$$

$$\lambda^2 + \frac{1}{rC} \lambda + \frac{1}{LC} = 0 \rightarrow \Delta = \frac{1}{r^2 C^2} - \frac{4}{LC} = \frac{1}{r^2 C^2} \left(1 - \frac{4R^2 C}{L} \right)$$

$$\lambda_{1,2} = \frac{-\frac{1}{rC} \pm \frac{1}{rC} \sqrt{1 - \frac{4R^2 C}{L}}}{2} = -\frac{1}{2rC} \left(1 \pm \sqrt{1 - \frac{4R^2 C}{L}} \right)$$

teraz niejednorodne: $I_1 = A_1 e^{\lambda_1 t} + B_1 e^{\lambda_2 t} + D_1$

$$\frac{D_1}{LC} = \frac{\varepsilon}{rLC} \rightarrow D_1 = \frac{\varepsilon}{r} \rightarrow I_1 = A_1 e^{\lambda_1 t} + B_1 e^{\lambda_2 t} + \frac{\varepsilon}{r}$$

Warunki początkowe: 1) brak prądu na starcie w cewce
 $I_1(0) = 0, Q_2(0) = 0$ 2) rozładowany kondensator

$$1 \rightarrow A_1 + B_1 = -\frac{\varepsilon}{r} \rightarrow B_1 = -\left(\frac{\varepsilon}{r} + A_1\right)$$

$$2 \rightarrow Q_2 = LC \partial_t I_1 \text{ (z BCDE)} \rightarrow \partial_t I_1 = 0 \rightarrow \lambda_1 A_1 - \lambda_2 \frac{\varepsilon}{r} - \lambda_2 A_1 = 0$$

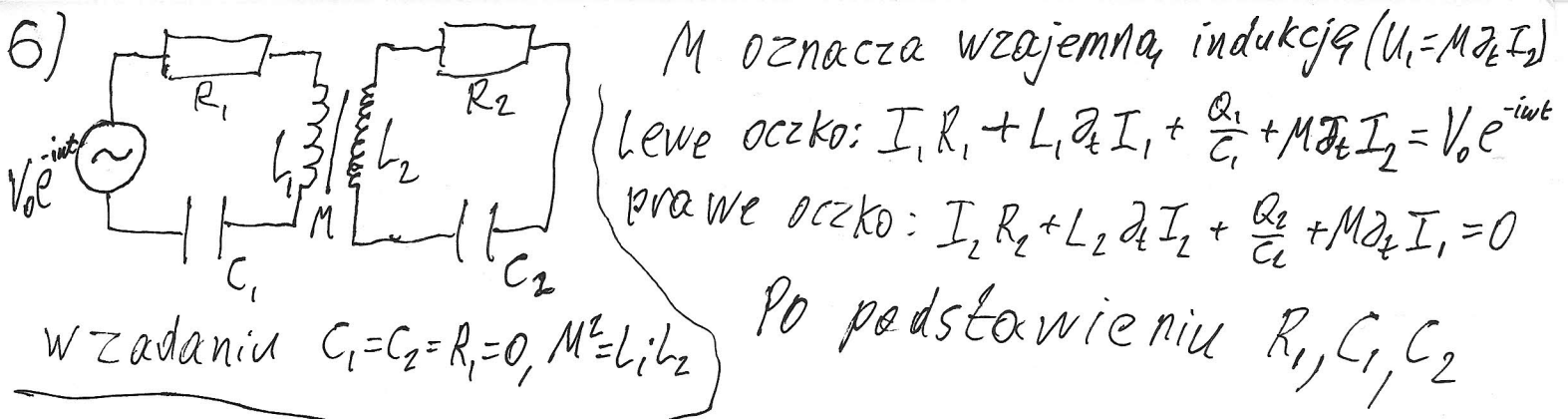
$$\cancel{A_1 = \frac{\lambda_1 - \lambda_2}{\lambda_1 - \lambda_2}} \quad (\lambda_1 - \lambda_2) A_1 = \lambda_2 \frac{\varepsilon}{r} \rightarrow \boxed{A_1 = \frac{\lambda_2}{\lambda_1 - \lambda_2} \frac{\varepsilon}{r}} \text{ reszta do wyznaczenia}$$

Popatrzmy uważnie na prąd: $I_1 = A_1 e^{\lambda_1 t} - A_1 e^{\lambda_2 t} + \frac{\varepsilon}{r} (1 - e^{\lambda_1 t})$

$$\left. \begin{aligned} \lambda_1 &= \frac{-1}{2rC} + \frac{\sqrt{1 - \frac{4R^2 C}{L}}}{2rC} < 0 \\ \lambda_2 &= \frac{-1}{2rC} - \frac{\sqrt{1 - \frac{4R^2 C}{L}}}{2rC} < \lambda_1 < 0 \end{aligned} \right\} \rightarrow A_1 e^{\lambda_1 t} - A_1 e^{\lambda_2 t} = A_1 e^{-\frac{t}{2rC}} \left(e^{\frac{\sqrt{1 - \frac{4R^2 C}{L}} t}{2rC}} - e^{-\frac{\sqrt{1 - \frac{4R^2 C}{L}} t}{2rC}} \right) = A_1 e^{-\frac{t}{2rC}} \cdot 2 \sinh \left[\frac{\sqrt{1 - \frac{4R^2 C}{L}} t}{2rC} \right]$$

czyli prąd ma zanikające oscylacje i prąd zbiegający do opornikowego

$$I = A \cdot e^{-\frac{t}{2rC}} \cdot 2 \sinh \left[\frac{\sqrt{1 - \frac{4R^2 C}{L}} t}{2rC} \right] + \frac{\varepsilon}{r} \left[1 - e^{-\frac{\sqrt{1 - \frac{4R^2 C}{L}} t}{2rC}} \right]$$



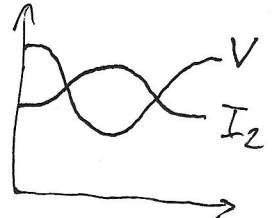
$$\begin{cases} L_1 \frac{dI_1}{dt} + M \frac{dI_2}{dt} = V_0 e^{-i\omega t} \\ L_2 \frac{dI_2}{dt} + M \frac{dI_1}{dt} + I_2 R_2 = 0 \end{cases} \rightarrow \frac{dI_1}{dt} = \frac{V_0 e^{-i\omega t} - M \frac{dI_2}{dt}}{L_1}$$

$$L_2 \frac{dI_2}{dt} + \frac{M V_0}{L_1} e^{-i\omega t} - \frac{M^2}{L_1} \frac{dI_2}{dt} + I_2 R_2 = 0$$

$$\left(\frac{dI_2}{dt} - \frac{M^2}{L_1 L_2} \frac{dI_2}{dt} \right) + \frac{M V_0}{L_1 L_2} e^{-i\omega t} + \frac{I_2 R_2}{L_2} = 0$$

przy $M^2 = L_1 L_2 \rightarrow 0$

$$I_2 = - \frac{M V_0}{L_1 R_2} e^{-i\omega t} = \underbrace{\frac{M V_0}{L_1 R_2}}_{\text{amplituda}} e^{-i\omega t} \underbrace{e^{i\pi}}_{\text{faza - przesunięcie o } 180^\circ}$$



czyli płynący prąd

$$I_2 = \text{Re}(I_2) = - \frac{M V_0}{L_1 R_2} \cos(\omega t)$$

$$P_2 = I_2^2 R_2 \text{ (z Joule'a)} = \frac{M^2 V_0^2}{L_1^2 R_2} \cos^2(\omega t) = \frac{L_2}{L_1 R_2} V_0^2 \cos^2(\omega t)$$

$$\text{średnia moc na 1 okres: } \langle P_2 \rangle = \frac{1}{T} \int_0^T P dt = \frac{\omega}{2\pi} \int_0^{2\pi/\omega} \frac{L_2 V_0^2}{L_1 R_2} \cos^2(\omega t) dt$$

$$= \boxed{\frac{L_2 V_0^2}{2 L_1 R_2}}$$

7)

H - Z Ampera (uwaga, Amper w ośrodku $\rightarrow \oint \vec{H} d\vec{s} = \iint \vec{J}_{\text{free}} d\vec{s}$)

$$H = \frac{I}{2\pi r} \rightarrow B = \begin{cases} \frac{\mu_0 I}{2\pi r}, & \text{w powietrzu} \\ \frac{\mu \mu_0 I}{2\pi r}, & \text{w cieczy} \end{cases} \rightarrow W = \iiint \frac{\vec{B} \cdot \vec{H}}{2} dV$$

$$W_{\text{MAG}} = \int_a^b dr \int_0^{2\pi} r d\varphi \left[\int_0^z dz \frac{\mu_0 (I/2\pi r)^2}{2} + \int_z^H dz \frac{\mu_0 (I/2\pi r)^2}{2} \right] =$$

$$= \ln \frac{b}{a} \cdot 2\pi \cdot \frac{I^2}{4\pi^2} \cdot \frac{\mu_0}{2} (H + (\mu z)) = \frac{\mu_0 I^2 \ln \frac{b}{a}}{4\pi} (H + (\mu z)) \rightarrow F_{\text{MAG}} = \partial_z W_{\text{MAG}} = \frac{\mu_0 \mu I^2}{4\pi} \ln \frac{b}{a}$$

$$W_{\text{grav}} = \rho V g \frac{z}{2} = \frac{\pi (b^2 - a^2)}{2} \rho g z \rightarrow F_{\text{grav}} = \partial_z W_{\text{grav}} = \frac{\pi (b^2 - a^2)}{2} \rho g z$$

$$F_g = F_M \rightarrow \left[z = \frac{\mu_0 \mu I^2 \ln \frac{b}{a}}{4\pi^2 \rho g (b^2 - a^2)} \right] \text{ ważne: } \mu \text{ może być mniejsze od 1, wtedy wypychamy}$$

przepraszam